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METHOD OF IZOD IMPACT TEST FOR STEEL

BUREAU OF CEYLON STANDARDS

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This Standard does not purport to include all the necessary provisions of a contract.

SRI LANKA STANDARD METHOD OF IZOD IMPACT FOR STEEL

FOREWORD

This Sri Lanka Standard Method of Test has been prepared by the Drafting Committee on Steel. It was approved by the Civil Engineering Divisional Committee of the Bureau of Ceylon Standards and was authorised for adoption and publication by the Council of the Bureau on 1975-07-02.

This standard is one of the Sri Lanka Standards on Methods of Impact Test. The other standard is SLS 355 Method of Charpy Impact (U-Notch) Test.

This standard is based on ISO Recommendation ISO-R 84 Izod Impact Test for Steel. All values given in this standard are in metric units.

1 SCOPE

This Sri Lanka Standard covers the test requirements and procedure of the Izod Imapct Test.

2 PRINCIPLE OF TEST

The test consists in breaking by one blow from a swinging hammer, under conditions defined hereafter, a notched test piece, gripped vertically, with the bottom of the notch in the same plane as the upper face of the grips. The blow is struck on the same face as the notch at a fixed position. The energy absorbed is determined and from this the impact value is deduced.

3 TEST PIECES

- 3.1 The test piece is of square or round section, unless otherwise specified.
- 3.2 The test piece conforms to the dimensions given in the following figures:
- a) Square test pieces: single-notch, Figure 1)

two-notch Figure 2)

three-notch Figure 3)

b) Round test pieces: single-notch Figure 5)

two-notch Figure 6)

three-notch Figure 7)

- 3.3 In each case, the plane of symmetry of the notch is perpendicular to the longitudinal axis of the test piece. The surface of the test piece should be smooth and free from grooves running parallel to the plane of symmetry of the notch.
- 3.4 The notch is of V-form having an included angle of 45° . The notch may be made by any machining method. The notch should be carefully prepared so that no grooves appear at the base of the notch.

3.5 Square test pieces

The notch is 2 mm deep with a root radius of 0.25 mm (Fig. 4).

3.5.1 The tolerances given in Table 1 are permitted.

3.6 Round test pieces

The notch is 3.30 mm (0.13 in) deep at the position of its maximum depth in the specimen. It has a root radius of 0.25 mm (Fig. 8).

TABLE 1 - Tolerances on specified dimensions

Designation	Nominal dimensions	Machining to	lerances
		Values	ISA symbols
Minimum length:			
single-notch	75 mm		
two-notch	100 mm		
three-notch	130 mm		1
Thickness	10 mm	± 0.11 man	j 13
Width	10 mm	± 0,11 mm	j 13
Angle of notch	45 ⁰	± 2°	-
Depth below notch	8 mm	± 0.045 mm	j 11
Distance of notch from end of test piece and from adjacent notch	28 mm	± 0.42 mm	j 15
Angle between plane of symmetry of notch and the longitudinal axis of the	· ·	± 2°	
test piece	90°	1 2	
	*		

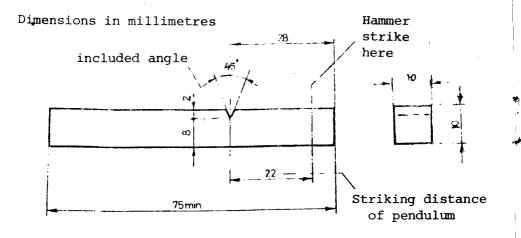


FIG. 1 Single-notch square test piece

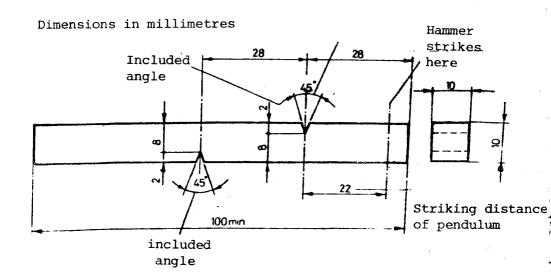


FIG. 2 Two-notch square test piece

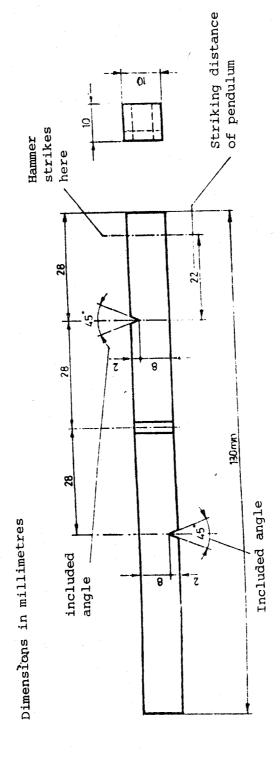


FIG. 3 Three-notch square test piece

Dimensions in millimetres

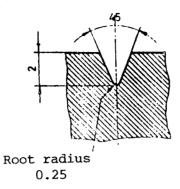


FIG. 4 Enlarged view of notch for square test piece

Dimensions in millimetres

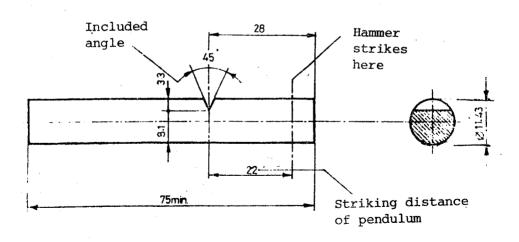


FIG. 5 Single-notch round test piece

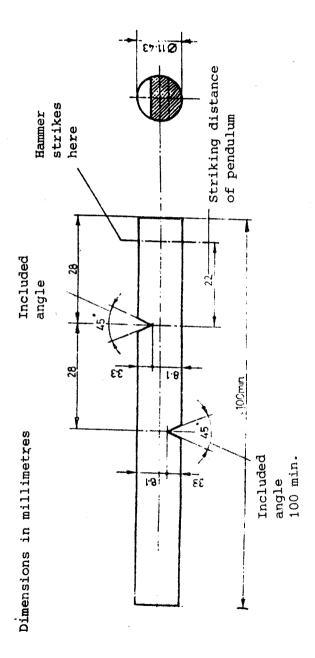


FIG. 6 Two-notch round test piece

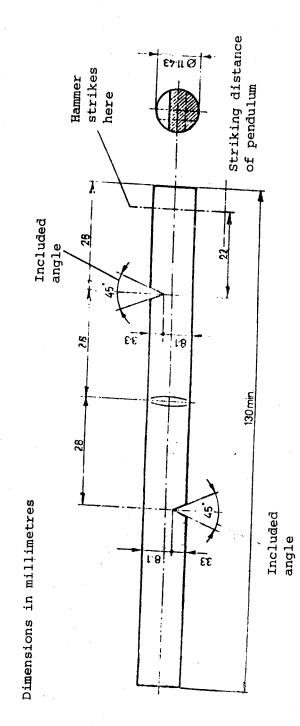


FIG. 7 Three-notch round test piece

TABLE 2 Tolerances on specified dimensions

Designation	Nominal dimension	Machining tolerance	ø
		Values ISA symbols	w
Minimum length:			
single-notch two-notch three-notch	76.2 mm (3 in) 104.1 mm (4.1 in) 132.1 mm (5.2 in)		
Diameter	11.43 mm (0.45 in)	± 0.14 mm j (± 0.005 in)	13
Angle of notch	450	1+ 50	ı
Depth below notch	8.128 mm (0.32 in)	+ 0.045 mm j (+ 0.002 in)	j 11
Distance of notch from end of test piece and from adjacent notch	27.94 mm (1.1 in)	± 0.42 mm j (± 0.018 in)	15
Angle between plane of symmetry of notch and longitudinal axis of test piece	006	1+ 50	

3.6.1 The tolerances given in Table 2 are permitted.

4 TESTING MACHINE

- 4.1 The testing machine is constructed and installed steady and rigid.
- 4.1.1 The conditions given in Table 3 should be satisfied.
- 4.1.2 The mass of the anvil and its foundation is at least 40 times the mass of the hammer.
- 4.1.3 The plane of swing of the hammer is vertical. The machine is constructed so that the loss of energy (such as from translation, rotation or vibration) in the machine framework during a test is negligible.
- 4.1.4 The centre of percussion is at the point of impact of the hammer.
- 4.1.5 The accuracy of the graduation of the scale of the machine is \pm 0.14 kgf m (\pm 1 lbf ft).
- 4.1.6 In addition, the machine should satisfy the conditions stated in Figures 9 and 10.

NOTE - The following relationships have been used for the conversion of metric units into foot and pound units.

5 TEST REQUIREMENTS

- 5.1 The longitudinal axis of the test piece should lie in the plane of swing of the centre of gravity of the hammer.
- 5.2 The notch should be positioned so that its plane of symmetry coincides with the top face of the grips.

TABLE 3 Characteristics of testing machine

Designation	Metric units	Foot and pound units
Distance between base of notch (top of grips) and point of specimen hit by striker (L of Fig. 9)	22 mm ± 0.5 mm	0.822 in ± 0.020 in
Angle between top face of grips and face holding the specimen vertical	₀ 06	06
Angle at tip of hammer	75°	750
Angle between normal plane to specimen and underside face of hammer at striking point	100	100
Speed of hammer at impact	3 to 4 m/s	9.8 to 13.1 ft/s
Striking energy	16.56 kgf m ± 0.34 kgf m	120 lbf ft ± 2.5 lbf ft

Dimensions in millimetres

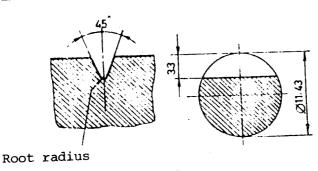


FIG. 8 Enlarged view of notch for round test piece

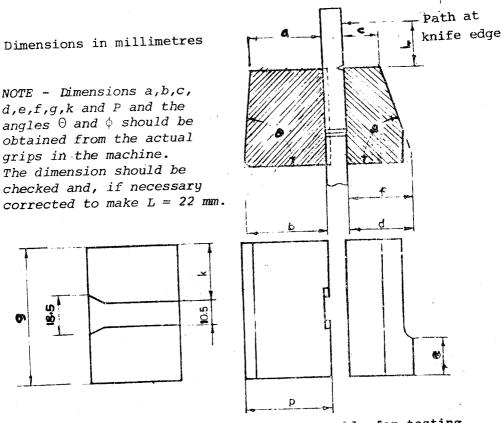
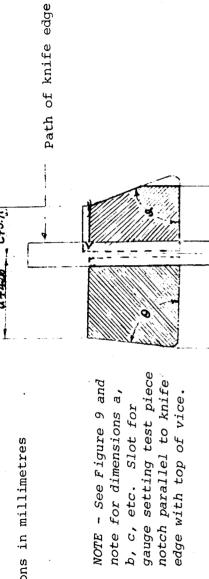
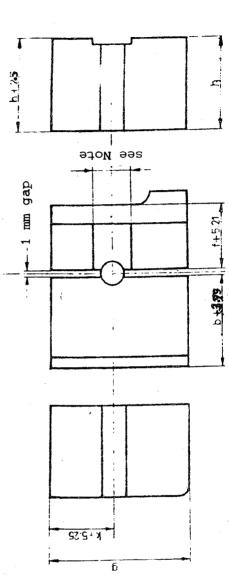


FIG. 9 View of grips and mode of assembly for testing square specimens





View of grips and mode of assembly for testing round specimens FIG. 10

- 5.3 The notch should be at right angles to the plane of swing of the centre of gravity of the hammer. This is ensured by the form of the test piece and the method of grip.
- 5.3.1 The test piece should be griped tightly in the anvil grips.
- 5.4 During testing of the two and three-notch pieces, the material remaining for testing after each test should be examined to ensure that the correct length of test piece is available above the next notch, and any undesirable deformed metal should be removed to ensure that the form and length of the test piece are correct before further testing
- 5.5 The impact value is quoted in foot-pounds-force or kilogrammes-force-metre (1 kgf m is equivalent to 7.233 ft lbf).
- 5.6 The temperature of the test piece at the moment of breaking should not differ from the specified temperature by more than ± 2 °C, unless some other tolerance is agreed. If the temperature of testing is not specified, it should be taken as 20 °C in temperate climates and 27 °C in tropical climates, subject in each case to the above tolerance. In all cases the temperature of test is to be recorded.
- 5.7 If, during the test, the test piece is not completely broken, the impact value obtained is indefinite. The test report should state that the test piece was unbroken by $x \text{ kgf m/cm}^2$ (ft lbf/in²).

NOTE - There is no general process for converting the impact values, obtained by one method of test, into those which would be obtained by another method of test.

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